

稠油原位气化制氢影响因素及机理

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摘要:针对稠油原位气化制氢(ISG)反应机理不明及蒸汽辅助重力泄油(SAGD)汽腔和火烧油层余热制氢可行性待验证等关键问题,通过高温、高压反应釜实验,系统探究了不同气氛(空气/氮气/二氧化碳)、不同温度(200~300℃)以及使用相同砂岩岩心粉末催化剂对稠油制氢的影响。采用多气氛控压恒温实验,反应恒压4 MPa,反应时间为6 h,结合气体质谱分析,揭示了200~300℃低温区间的制氢潜力与反应机理。结果表明:①氮气氛围在300℃时产氢最优(浓度4.4%),其惰性特性避免了氢气消耗,而二氧化碳气氛下制氢效率较低,主要因二氧化碳与稠油反应生成一氧化碳,消耗部分氢气;②温度主导制氢可分为3个阶段,150~250℃为启动期,250~300℃为热解期,大于300℃为高效期;③岩心粉末在氮气下催化效果显著,产氢量提升33%,证实地层矿物对低温制氢的促进作用。研究阐明不同条件下的制氢机理,为稠油资源绿色转化提供了新策略。

关键词:反应釜;催化;氢气;稠油;水-煤气变换;焦炭

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Influential factors and mechanisms of hydrogen production via in-situ heavy oil gasification

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Abstract: This study aims to determine the reaction mechanisms behind the in-situ gasification (ISG) of heavy oil and assess the feasibility of hydrogen production using exhaust heat from the steam chamber of steam-assisted gravity drainage (SAGD) and from in-situ combustion. Through experiments with a high-temperature high-pressure (HTHP) autoclave, we systematically explore the impacts of different atmospheres [air, nitrogen (N_2), and carbon dioxide (CO_2)], varying temperatures (200 °C to 300 °C), and core powder catalysts of the same sandstone sample on hydrogen production from heavy oil. Using experiments with a fixed pressure (4 MPa), constant temperatures, and a reaction time of 6 h under multiple atmospheres, as well as mass spectrometry, we reveal the potential and reaction mechanisms of hydrogen production under low temperatures ranging from 200 °C to 300 °C. The results show that the N_2 atmosphere yields the highest hydrogen production performance (hydrogen concentration: 4.4%) at a temperature of 300 °C attributed to the inert nature of N_2 , which inhibits hydrogen consumption. In contrast, the CO_2 atmosphere shows relatively low hydrogen production efficiency. This occurred primarily because CO_2 reacted with heavy oil to generate CO, thereby consuming part of the available hydrogen. The temperature-dependent hydrogen production process can be divided into three stages: the initial stage (150 °C to 250 °C), the pyrolysis stage (250 °C to 300 °C), and the high-efficiency stage (above 300 °C). Under the N_2 atmosphere, core powder demonstrates a significant catalytic effect, increasing hydrogen production by 33%. This highlights the role of formation minerals in promoting low-temperature hydrogen production. This study clarifies the hydrogen production mechanisms under different conditions, providing a novel strategy for converting heavy oil into green resources.

Key words: autoclave, catalysis, hydrogen, heavy oil, water-gas shift (WGS) reaction, coke

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氢气作为一种绿色能源,由于其可再生、零排放的特性,被广泛认为是减少空气污染物和温室气体排放的有效手段^[1–7]。氢气的生产方式多样,主要包括煤制氢、天然气重整制氢以及化工副产品制氢。目前,煤制氢和天然气重整制氢技术主导全球市场,其中约18%的氢气来自煤炭,48%来自天然气重整,30%来自石油炼化^[8–11]。在此背景下,石油工程领域近年来提出了稠油原位气化(ISG)制氢技术,尤其适合稠油资源丰富的地区。全球油砂储层中的稠油和沥青储量超过 6×10^{12} bbl,使其成为世界第三大非常规石油资源^[12]。原位气化技术利用稠油作为制氢原料,将地下地层视为天然的高温、高压反应釜,将难以开采的稠油转化为氢气和甲烷等清洁能源,同时提高稠油采收率^[13–14]。

稠油原位气化在实验室及部分现场项目中已展现出可行性。典型的稠油原位气化应用案例为艾伯塔玛格利特湖项目。该项目通过蒸汽吞吐及注空气氧化燃烧等方法实现稠油原位气化制氢,产出气体中最高体积掺氢比可达20%^[15]。Belgrave等^[16]的研究采用拟组分反应模型,揭示了稠油原位燃烧(ISC)的复杂机制,该模型涵盖了软沥青、沥青质、焦炭和天然气4种组分,并包含热裂解、低温氧化(LTO)和高温氧化(HTO)等6种反应过程。Kapadia等^[17]基于Strausz和Phillips的实验数据,利用阿伦尼乌斯法计算了沥青热裂解的动力学参数,并改进了Yang和Gates的动力学氧化模型^[18],将氢的生成与消耗反应纳入其中。Hajdo等^[19]指出,玛格利特湖油砂稠油的氢气主要源于焦炭气化、水-煤气变换、热解和水热裂解反应。Yang等^[20]通过热重-质谱联用技术研究了稠油的热解产氢机制,发现444 ~ 528 °C区间内稠油热解会产生少量氢气和轻质烷烃,而当温度升高至528 ~ 900 °C时,则进入焦炭脱氢阶段,产氢量显著增加。He等^[21]的研究表明,重油中树脂含量对氢气产量影响最大,其次是沥青质含量,且在缺氧条件下更有利于氢气的生成。王田田等^[22]通过燃烧管实验,证实了注蒸汽开发后稠油油藏火驱原位制氢的可行性。陈莉娟等^[23]研究了温度、含

水饱和度、氧气体积分数和压力对新疆油田红浅稠油原位气化制氢影响,揭示了高效产氢的条件。

目前,已初步建立了稠油原位气化的反应体系和动力学模型,并验证了其机理,但仍存在一些亟待解决的问题:大多数研究集中在450 °C以上的制氢反应,稠油蒸汽辅助重力泄油(SAGD)汽腔温度在250 °C左右,该温度下能否制氢、反应机理是什么,目前尚未见到报道;温度、压力和反应时间等外部因素对稠油制氢过程的影响亦有待系统研究。为填补这些研究空白,本研究设计了高温、高压反应釜实验,选择不同气氛(空气、氮气和二氧化碳)在多温区间进行恒温、恒压实验,并收集气体产量数据进行对比分析。本研究深化了稠油原位气化制氢机理,明确了蒸汽辅助重力泄油汽腔余热制氢的可行性和影响因素,为丰富氢能生产方式提供了理论支撑。

1 实验材料与方法

本研究所采用的油样CA-28为加拿大稠油,其4种组分的含量分别为:饱和烃23.42%,芳香烃23.09%,胶质35.41%,沥青质10.15%。其中,胶质与沥青质含量总和占组分总量近一半,是造成该稠油黏度极高的原因之一。为了使实验数据更接近实际地层反应,选取岩心粉末作为催化剂,并对催化剂进行元素分析,认识到岩石粉末中含有铁、钴和镍等常见的金属催化剂(表1)。实验选用氮气、空气和二氧化碳3种不同气体作为实验的反应气氛。

采用高温、高压反应釜进行恒温实验,利用气体质谱分析仪(MS)进行产气检测(图1)。反应样品按照油、水、气体积比为1.5:1.5:97.0进行配比,首先称量油样CA-28、去离子水与岩心粉末量,向反应釜中加入油样0.80 g、去离子水0.80 g以及岩心粉末0.08 g,搅拌均匀后密封反应釜。通过抽真空排除釜内残余气体,以空气、氮气和二氧化碳3种气体作为反应气氛,打开气瓶向反应釜中泵入气体。注气完成后关闭反应

表1 高温、高压反应釜产氢实验中稠油样品岩心粉末元素分布统计

Table 1 Statistics of mass proportions of various elements in the core powder of the heavy oil sample in a hydrogen production experiment in a HTHP autoclave

元素	碳	氧	硅	镁	铝	钙	铁	钴	镍
质量分数/%	6.91	37.42	30.81	0.10	15.73	0.29	5.95	1.25	1.54

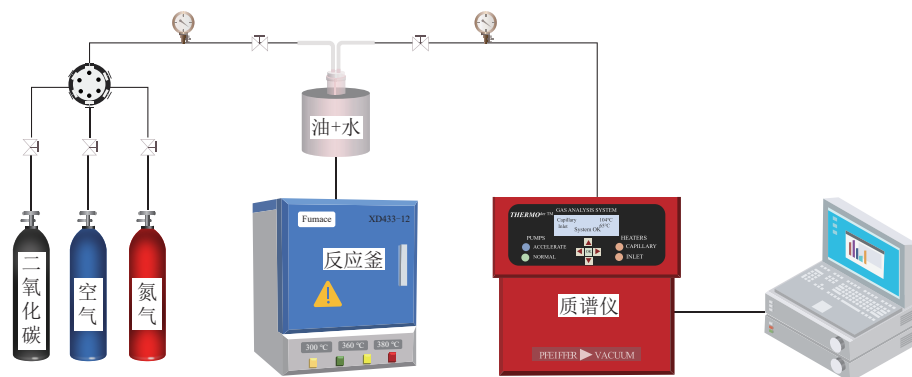


图1 高温、高压反应釜产氢实验设备示意图

Fig. 1 Experimental setup with a HTHP autoclave used for hydrogen production

表2 高温、高压反应釜产氢实验条件设计

Table 2 Designed experimental conditions for a hydrogen production experiment in a HTHP autoclave

反应气氛	实验材料	反应温度/℃	注气压力/MPa
空气	油+水	200	1.4
	油+水	250	0.9
	油+水	300	0.5
	油+水+岩心粉末	200	1.4
	油+水+岩心粉末	250	0.9
	油+水+岩心粉末	300	0.5
氮气	油+水	200	1.4
	油+水	250	0.9
	油+水	300	0.5
	油+水+岩心粉末	200	1.4
	油+水+岩心粉末	250	0.9
	油+水+岩心粉末	300	0.5
二氧化碳	油+水	200	1.4
	油+水	250	0.9
	油+水	300	0.5
	油+水+岩心粉末	200	1.4
	油+水+岩心粉末	250	0.9
	油+水+岩心粉末	300	0.5

釜阀门,将反应釜放入马弗炉中,马弗炉升温速率为 $10\text{ }^{\circ}\text{C}/\text{min}$,设定恒温时间为 6 h ,恒温温度为 $200, 250$ 以及 $300\text{ }^{\circ}\text{C}$ 。根据实验设定,到达目标温度后的反应釜内压力为 4 MPa 。利用集气袋对反应釜内产生的气体进行收集,将集气袋中的气体稳定输入质谱仪中,对气体组成进行检测。本实验测定了3种气氛、3个温度下共18组反应气体(表2)。

2 实验结果分析

经过高温、高压反应釜进行恒温水热反应后,稠油气态产物组成结果如表3所示(数据已归一化处理)。结果表明,生成的气体主要由甲烷、高分子量气体

(HMWG,指 C_{2+} 烃类气体)、氮气、硫化氢、一氧化碳和二氧化碳组成,这与Muneer和Jiménez等^[24-25]的反应釜实验数据一致。需要注意的是,二氧化碳气氛实验中,由于二氧化碳被消耗,未统计该系列实验中的二氧化碳产量。

图2指示在空气、氮气和二氧化碳3种气氛下产生的氮气、甲烷、硫化氢和高分子量气体的浓度(体积分数)。当温度低于 $250\text{ }^{\circ}\text{C}$ 时,空气和二氧化碳气氛中产生的氮气浓度均高于氮气气氛中产生的氮气浓度。这是由于空气气氛中的氧化反应属放热反应,提升了反应釜的内部温度,从而促进了低温条件下的氮气产出。在二氧化碳气氛中,充足的二氧化碳与稠油中的烃类进行重整反应^[26],并与稠油热解产生的焦炭发生气化反应,焦炭被还原,从而产生大量的一氧化碳^[27](表3),这也促进了水-煤气变换反应的充分进行,使低温下的氮气浓度达到最高。当温度升高至 $300\text{ }^{\circ}\text{C}$ 时,空气气氛中的氮气浓度为 0.93% ,而二氧化碳气氛下的氮气浓度为 1.21% ,氮气气氛下的氮气浓度则为 3.30% ,是3种气氛中最高的。这表明,在空气气氛中,由于氧气的存在,一部分氢气被氧化,而在二氧化碳气氛中,氮气浓度的增加相对较小,说明高浓度的二氧化碳对氢气生成反应的抑制效应在高温下更加显著^[28]。与此相比,氮气气氛下则不存在明显的耗氢或抑制反应,使得该气氛下的氢气浓度达到最高。

从气体产出组成分布来看,3种气氛在低温条件下产生的甲烷体积占比最大,说明在 $250\text{ }^{\circ}\text{C}$ 以下,稠油的主要反应为物理挥发及胶质与沥青质等大分子的初步热解,导致气体中甲烷含量较高。当温度升至 $300\text{ }^{\circ}\text{C}$,稠油的热解与水热反应更加剧烈,导致大分子支链断裂^[29],从而产生更多的轻烃,高分子量气体的产量明显提升,而甲烷的浓度则相应降低。在二氧化碳气氛下,由于二氧化碳的存在,许多热解反应逆向发生,降低了

表 3 高温、高压反应釜产氢实验中稠油产气数据统计

Table 3 Statistics of gas composition produced from heavy oil in the HTHP autoclave

反应气氛	反应条件	产出气体的体积分数/%					
		H ₂	CH ₄	H ₂ S	HMWG	CO	CO ₂
空气	200 ℃	0.56	96.88	0.27	1.94	0.07	0.28
	200 ℃ + 催化	0.56	95.57	0.27	1.96	1.32	0.32
	250 ℃	0.54	94.85	0.65	2.40	0.98	0.57
	250 ℃ + 催化	0.78	93.34	0.78	3.82	0.63	0.65
	300 ℃	0.93	79.85	2.49	13.16	1.27	2.30
	300 ℃ + 催化	1.04	67.40	1.81	15.74	1.83	12.18
氮气	200 ℃	0.45	97.03	0.34	2.08	0.02	0.08
	200 ℃ + 催化	0.60	94.63	0.56	3.27	0.41	0.54
	250	0.48	95.70	0.32	2.14	1.09	0.28
	250 ℃ + 催化	0.46	95.58	0.35	2.11	1.26	0.24
	300 ℃	3.30	58.05	2.28	25.15	4.81	6.42
	300 ℃ + 催化	4.44	47.54	3.18	25.72	4.94	14.16
二氧化碳	200 ℃	0.69	84.59	0.49	2.26	11.96	—
	200 ℃ + 催化	1.08	70.29	0.74	3.82	24.06	—
	250 ℃	1.18	70.33	0.99	3.57	23.92	—
	250 ℃ + 催化	1.29	63.67	1.03	5.12	28.89	—
	300 ℃	1.21	59.70	1.06	2.94	35.09	—
	300 ℃ + 催化	1.29	62.74	1.05	3.48	31.44	—

注：“—”表示未统计。HMWG 指高分子量气体。

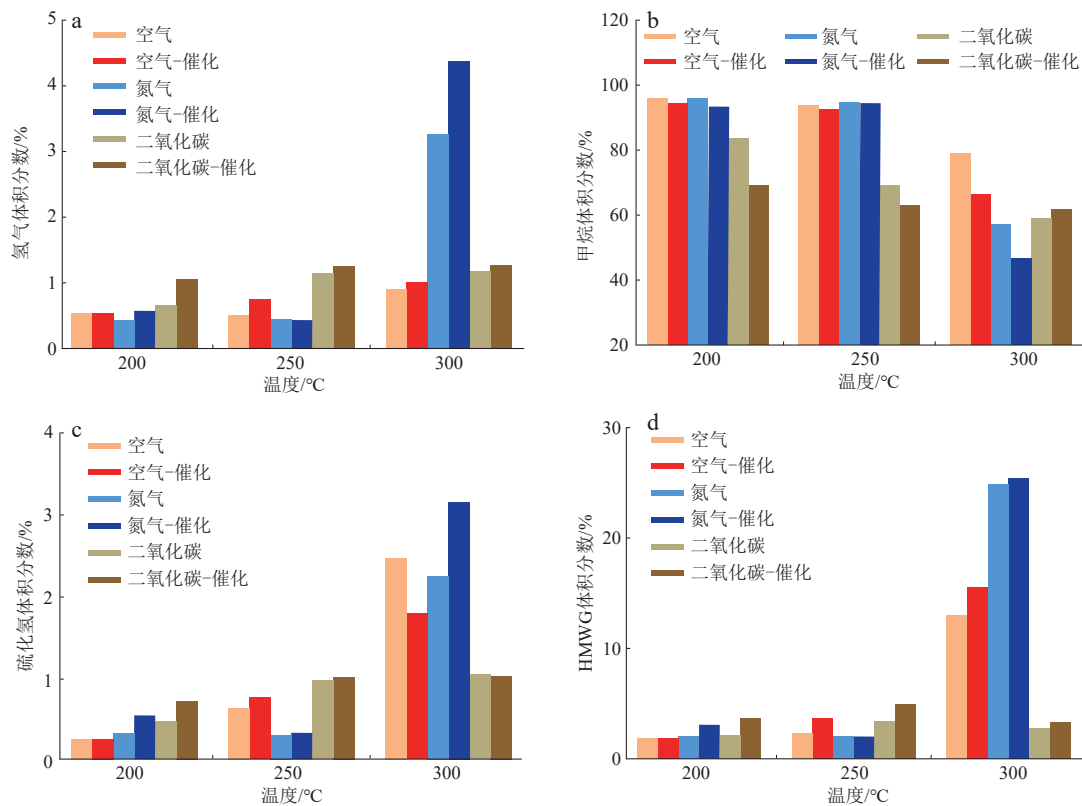


图 2 高温、高压反应釜产氢实验中不同温度下空气、氮气及二氧化碳 3 种气氛中产出的氢气(a)、甲烷(b)、硫化氢(c)以及高分子量气体(HMWG)(d)体积分数分布柱状图

Fig. 2 Columns of volume proportions of hydrogen (a), methane (b), hydrogen sulfide (c), and higher-molecular-weight gas (HMWG) (d) produced in air, N₂, and CO₂ atmospheres at diverse temperatures in a hydrogen production experiment in a HTHP autoclave

热解反应的效率^[30],导致高分子量气体浓度没有显著变化,同时,二氧化碳与稠油热解沉积的焦炭结合生成大量一氧化碳,进一步影响了反应的动态平衡。

在不同反应气氛中,该实验所选用的岩心粉末均起到了催化产氢的效果,且其中氮气气氛下的催化效果最为显著。在300℃条件下,催化前的氢气浓度为3.3%,催化后氢气浓度提升至4.4%。岩石粉末中含有铁、镍及钴等重金属元素,其中,铁元素是水-煤气变换反应的重要催化剂,可以降低反应的活化能,从而进一步提升产氢量^[31]。镍能够催化重碳氢化合物裂解形成自由基^[32],而钴催化剂有效地破坏稠油中重质组分的C—C、C—S和C—O等化学键,促进这些组分转化为较轻质的烃类^[33]。

3 制氢与耗氢机理

基于本次实验研究及前人的研究成果,提出稠油制氢与耗氢机理(图3)。稠油组成复杂,将其作为整体进行研究难以准确揭示其制氢的化学过程。因此,通常采用SARA分析法将稠油定量为4种主要的化学组分^[34](饱和烃、芳香烃、胶质和沥青质)进行研究。

在产氢启动阶段,稠油与水主要发生物理变化,包

括水吸热汽化为水蒸气,以及轻质烃类初步挥发。当温度达到约200℃时,羧基酮、醛和酯类化合物发生热分解^[35],生成低分子气态物质。随着温度升高,大分子化合物的支链C—C键断裂,形成短碳链烃类自由基和游离氢,进一步生成甲烷、乙烷及可冷凝的饱和和低碳烃。在加入水蒸气后,150~250℃范围内,通过稠油中的金属催化剂(主要是铜基催化剂)^[36-37]进行低温水-煤气变换反应。这一反应在低温下具有高氢选择性和较高的转化率^[38]。此时,醛类化合物的热解生成的一氧化碳作为水-煤气变换反应的原料^[39-40],与水蒸气发生置换反应,产生氢气和二氧化碳。

在热解产氢阶段,基于Greensfelder等^[41]的自由基反应理论及Sun等^[42]提出的脱氢反应机理,当温度升至250℃以上时,热解反应首先由沥青质的C—C键断裂引发,释放自由基^[43],进入热解的诱导期。自由基通过与其他分子的氢结合后再次诱发C—C键断裂,产生小芳烃和饱和物。Kun等^[44]研究表明,热解稠油过程中,胶质和沥青质会形成一定量的焦炭,表明这些重组分在焦化过程中具有高度反应性,进一步证实了胶质和沥青质是焦炭生成的主要贡献者。

在氢气高产阶段,产氢主要途径包括3类:环烷芳基烃的脱氢反应、胶质与沥青质的缩合反应以及高温

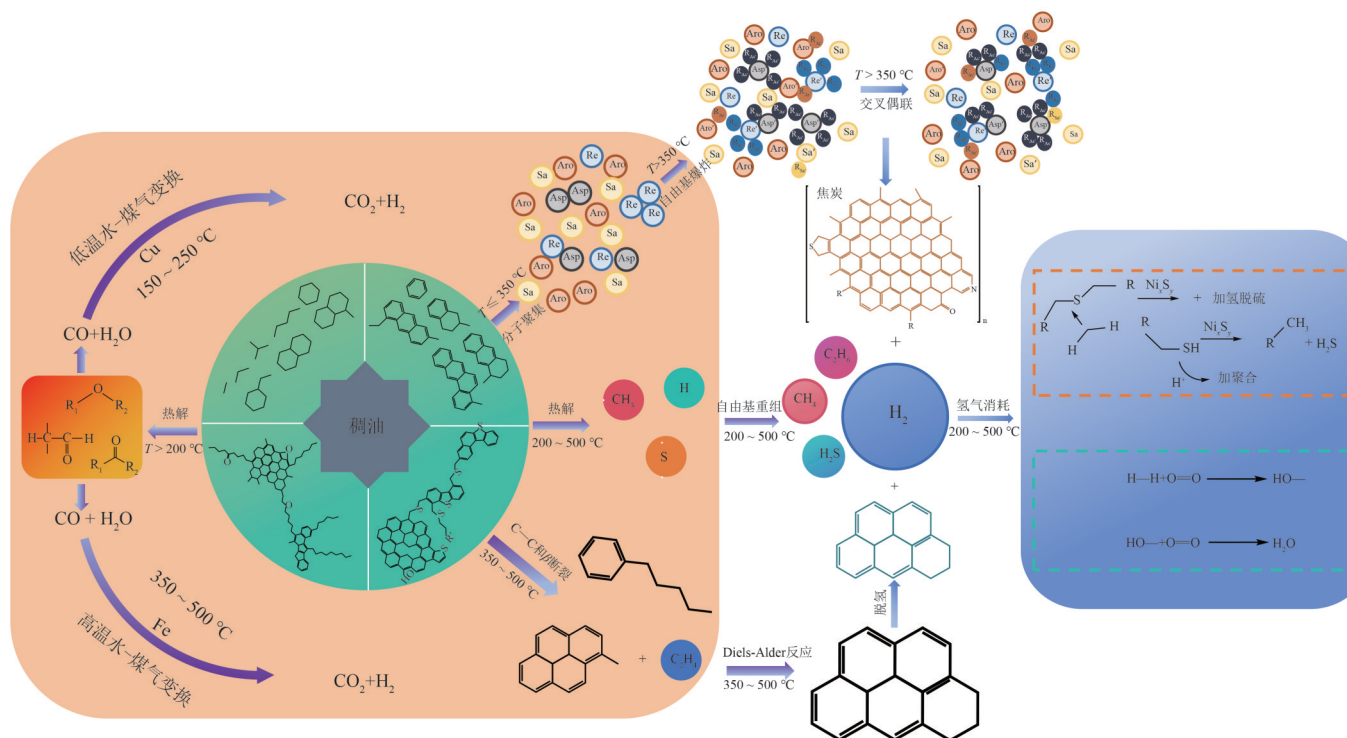


图3 稠油原位产氢与耗氢机理示意图

Fig. 3 Mechanisms underlying hydrogen production and consumption via the ISG of heavy oil

(Sa表示饱和烃;Aro表示芳香烃;Re表示胶质;Asp表示沥青质。)

水-煤气变换反应。随着热解过程的进行,当温度升至 350 °C 以上,缩合反应的趋势明显增强。该反应通过 C—C 键断裂和 β 断裂生成甲基化芳香自由基,与短链烯烃通过 Diels-Alder 反应生成环烷基芳烃,进而环烷基芳烃的脱氢产生氢气并转化为多环芳烃。连续的 Diels-Alder 反应生成大分子^[45-48]并增加沥青质体积占比,使其在反应体系中聚集,从而形成焦炭前体。稠油中的胶质和沥青质会产生大量自由基,这些自由基能够相互耦合形成新的凝聚结构,这些结构可进一步与大型多环芳烃聚集体结合,从而促进焦炭的生成并提高氢气产量。随着热解的进行,缩合反应逐渐加强,并开始与脱烷基化过程并行进行,可能会生成重馏分^[49],如沥青质甚至焦炭。在此阶段,铁基催化剂的存在使高温水-煤气变换反应更加剧烈,反应的吉布斯自由能随温度升高而增加,这表明高温对该反应不利^[50]。尽管在较高温度下转化率低于低温水-煤气变换反应,但因高温能增加分子碰撞频率,有利于一氧化碳的消耗,从而加快产氢速率。在上述反应中,产生的部分焦炭作为气化制氢的原料,同时也会将体系中的二氧化碳还原为一氧化碳,并且在该温度下,羰基和醚类化合物会达到热解温度^[51],生成大量的一氧化碳,从而推动水-煤气变换反应的进行。

在整个稠油制氢过程中,氢气的消耗同时存在。沥青质被认定为硫的主要来源,硫以硫醇、硫醚及噻吩等化合物形式存在^[52-53]。当温度超过 200 °C 时,硫化氢的产量显著增加^[54],这是因为有机硫化物(如噻吩和四氢噻吩)转化过程中通过从水分子中转移氢实现杂原子质子化,导致 C—S 键断裂^[55-56],从而产生氢气,促进噻吩的加氢脱硫反应及不饱和烃的加氢反应,通常在热解产氢阶段反应最为剧烈。在有氧气存在时,氧气会参与氢气的消耗,通过促进某些烃类的氧化反应消耗氢原子,或抑制氢气的生成。在热解过程中产生的游离氢在有氧气条件下可能会迅速与氧气反应生成水,减少氢气的生成。高温条件下,反应速率增加,氢自由基与氧气反应更为迅速^[57],氧气浓度也影响氢自由基的反应机制,高浓度的氧气将促进氢自由基的氧化。

4 结论

1) 储层岩屑粉末具有催化制氢的作用,并且在氮气气氛下的催化效果最为显著。实验观察显示,在氮气气氛下,在 300 °C 下反应 6 h 后氢气摩尔浓度为 3.3%,催化后的氢气摩尔浓度为 4.4%,而在空气气氛

和二氧化碳气氛下催化前、后的氢气浓度无明显变化,且氧气与二氧化碳的存在都会消耗氢气或抑制氢气的产生,氮气气氛作为惰性气体不参与反应,进一步增强了产氢效果。

2) 稠油热解产氢呈现阶段性特征。低温阶段(150 ~ 250 °C)以水-煤气变换反应、轻烃挥发及羧基化合物热解为主,铜基催化剂促进低温水-煤气变换高效产氢;中温阶段(> 250 °C)沥青质和胶质 C—C 键断裂引发自由基反应,生成低碳烃与焦炭前体;高温阶段(> 350 °C)脱氢、缩合反应及铁基催化高温水-煤气变换成为主要产氢途径,缩合反应增强焦炭生成,后者参与气化消耗二氧化碳并助推产氢。

3) 温度介于 150 ~ 450 °C 时的稠油原位制氢机理为,在产氢启动阶段羰基、醚键与醇类热解生成的一氧化碳促进低温水-煤气变换反应的进行,在热解产氢阶段沥青链 C—C 键断裂释放的自由基重组产生氢气,在氢气高产阶段通过环烷基芳烃脱氢反应、胶质与沥青质缩合反应以及高温水-煤气变换反应而大量产氢。

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