

加热过程中页岩储层改质效果研究进展

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摘要: 中国陆相页岩油资源潜力巨大,但因成熟度偏低、油质重、粘度大、地层流体压力低且孔渗条件差而难以有效开发。原位加热技术可显著提高其采收率,储层改质是该技术的重要目标之一。基于前人对页岩孔隙演化的研究以及对油页岩原位加热过程中储层物性改质的探索,通过理论分析,明确了储层改质效应由孔隙演化和热致裂两种机制控制。孔隙演化主要由有机质裂解、无机矿物成岩转化、矿物溶蚀和重结晶引起;热致裂主要由热应力和生烃增压造成。前期对不同成熟度页岩孔隙演化规律的研究以及对砂岩、花岗岩热破裂作用的研究,为进一步揭示页岩原位加热过程中的储层改质效应奠定了良好基础。但页岩中复杂的矿物成分导致其孔隙演化过程更加复杂,有机质裂解过程所伴随的成孔作用、酸性产物溶蚀作用以及增压效应使该过程进一步复杂化。在进一步研究中,需要对不同作用开展相对独立的研究,揭示其机理并建立预测模型,进而对原位加热过程中整个增孔增渗效应在时间和空间上的演化进行有效预测。

关键词: 孔隙演化;热致裂;热应力;原位加热;储层改质;提高采收率;页岩油

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Progress in shale reservoir upgrading through in-situ heating

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Abstract: Non-marine oil shale is abundant in China but most of it is not economically accessible due to its low maturity, low API gravity, high viscosity, low-pressure formation fluid as well as low porosity and permeability. In-situ heating technology has been used to improve the recovery rate of the oil and proven quite effective in improving the shale reservoir properties. Based on previous studies on shale pore evolution and reservoir property improvement through in-situ heating of oil shale, this study clarifies that the improvement of shale reservoir properties through heating is realized by both the pore evolution and the thermal cracking. Pore evolution is mainly facilitated by organic matter cracking, inorganic mineral transformation, mineral dissolution and recrystallization. Thermal cracking is mainly induced by thermal stress and hydrocarbon generation supercharging. Despite the insights gained from previous studies on pore evolution pattern of shale of different maturity and on thermal cracking in sandstone and granite, challenge remains in further revealing the effect of reservoir improvement in the in-situ heating process of shale because of the complex mineral composition in shale that leads to a more complex pore evolution process, which is further complicated by pore formation, acid product dissolution and supercharging effect associated with organic matter decomposition. It is therefore suggested that further research be carried out separately on each different effect to reveal the mechanisms and

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establish models, so as to effectively predict the temporal and spatial evolution of the entire pore and permeability enhancement effect during the in-situ heating process.

Key words: pore evolution, thermal cracking, thermal stress, EOR, in-situ heating, oil shale

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美国已凭借页岩油气革命性技术突破和成功的商业开发,从原油和天然气进口国变为出口国。然而,中国2020年原油对外依存度已上升至73%,已远超国际所公认的50%警戒线。在中国常规油气资源产量逐年下降之际,加大对页岩油气资源的勘探和开发力度有望提高当下国内油气产量,进而保障能源供给并优化调整能源结构^[1-6]。

自然资源部油气资源战略研究中心2012—2013年评价中国陆相页岩油地质资源量为 402×10^8 t,可采资源量为 37×10^8 t;中国石化2014年评价中国陆相页岩油地质资源量为 204×10^8 t;中国石油2017年评价中国中-高成熟度页岩油资源量为 132×10^8 t。尽管不同机构的评价存在一定差异,但就中国页岩油资源潜力巨大这一基本认识已达成共识。

尽管资源潜力巨大,但中国绝大多数陆相含油页岩的成熟度偏低,储层具有低孔、低渗的特征,加上页岩油分子大,并且具有极性高和含蜡等特点,导致其难以流动。尽管目前已经通过水力压裂等手段一定程度地增强了页岩储层孔隙连通性,但仍未获得理想产能^[3],亟需新理论、新技术和新方法的诞生和发展为中国陆相页岩油的有效开发开辟新途径^[7]。

国外在对油页岩开发时探索了原位加热改质技术^[8],与地面干馏相比,原位加热开采具有成本低、占地面积小、环境污染小的优势^[9-10]。目前,对页岩原位加热改质技术的探索主要包括电加热、蒸汽加热、电磁波加热等^[11-12],其中,壳牌公司探索的原位电加热技术最为成熟,加热工艺和关键设备等技术难题已基本得到解决,并在美国科罗拉多州、加拿大阿尔伯达省、约旦等地进行了38个井组现场试验,基本具备工业化应用条件^[13]。原位加热改质技术有望在未来的页岩油大规模商业化开采中起到关键作用。

与国外相比,国内对页岩原位加热改质技术的研究工作起步较晚,21世纪以来高校和科研单位才逐步开展相关研究,并且主要针对油页岩而非页岩油资源^[14-18]。对页岩油的探索近几年才刚刚开始,尚处于论证、探索和初步尝试阶段,对国外技术依赖性强,尚

未掌握核心机理,难以对原位加热过程中页岩储层和原油性质进行有效预测,更难对增产效果进行准确评估。

页岩原位加热原位改质过程中,有机质和无机矿物的物理-化学综合作用将导致页岩储层产生增孔致裂效应,大幅增强页岩孔和缝的连通性,改善页岩储层的渗透性^[19],并进一步提高页岩储层中油气的流动性和可采性。对原位加热过程中储层改质效果与波及范围的有效预测,是制定经济有效的加热方案的重要前提。然而,原位加热改质过程中的增孔致裂过程十分复杂,目前对其机理认识不清,加之中国陆相页岩储层非均质性极强^[20-22],进一步加大了对该过程的研究难度,为增孔致裂过程的有效预测以及加热方案的合理制定带来了巨大挑战。因此,在研究页岩油原位加热改质开采机理的过程中,页岩储层的增孔致裂机理是重要一环,也是目前研究的薄弱环节,亟需开展深入研究。

1 原位加热过程中页岩储层改质过程

页岩主要由有机质和无机矿物构成,有机质主要为干酪根和油气,无机矿物主要包括各类粘土、碳酸盐、石英和长石等^[23-24]。在原位加热改质过程中,页岩中的有机质和无机矿物将发生一系列物理和化学作用,导致其产生增孔和致裂效应。

1.1 页岩受热过程中的孔隙演化过程

高温高压条件将导致页岩发生一系列促进或抑制孔隙演化的成岩作用:①有机质生烃作用,有机质经初次和二次裂解生成油气,并伴随有机酸、 H_2S 和 CO_2 等酸性产物的生成^[25],与此同时,形成大量有机孔隙^[26];②无机矿物转化作用,比如粘土矿物从成分上由蒙脱石(或伊/蒙混层)向伊利石转化,形态上由片状向丝状、再向絮装转化,粘土矿物脱水收缩导致其晶间孔增加,有利于收缩缝的形成^[27];③溶蚀作用,有机质裂解生成的有机酸和 H_2S 等酸性物质使黄铁矿、碳酸

盐岩、粘土矿物、石英和长石等不稳定矿物发生溶蚀作用^[5,28],产生次生孔隙,但与此同时,可能会生成高岭土、透辉石等矿物,会造成一定程度的孔隙充填^[29];④重结晶作用,有机质裂解生成的 CO_2 导致携带 Ca^{2+} 的溶液在孔缝中重结晶而充填孔缝,导致页岩储集空间减少,但却使得页岩脆性增强,有利于增压致裂。

1.2 页岩受热过程中的致裂过程

根据热弹性力学理论,温度改变时,物体由于外在约束以及内在各部分之间的相互约束,使其不能完全自由胀缩而产生的应力为热应力^[30]。岩石受热时会产生热应力,热应力最大值往往发生在矿物颗粒的边界处,如果此处的热应力达到或超过岩石的强度极限(抗拉强度或抗剪强度),则沿此边界的矿物颗粒之间的连结处断裂并产生微裂纹,随着温度的升高,这些裂纹逐渐形成网络,即产生热破裂现象^[31-32]。对页岩进行原位加热改质时,页岩内部颗粒、孔隙与微裂纹的强度较低,将在局部产生应力集中,进而发生热破裂。现有研究表明,热破裂作用在原位加热改质页岩中起到了至关重要的作用^[33]。

2 原位加热中页岩储层改质作用研究进展

在原位加热过程中,页岩的增孔和致裂效应往往同时发生,在研究的过程中难以将二者完全剥离,尤其在采用低温液氮吸附、高压压汞、气测孔隙度等实验进行测试时,所测得的孔体积和孔隙度等参数是增孔和致裂作用的综合体现。

2.1 原位加热中页岩孔渗演化

在对烃源岩的生烃过程进行定量研究时,国内外学者已经分别从实验模拟和数值模拟方面开展了大量研究。实验模拟方面,基于时温互补原理分别开发了开放体系、封闭体系和半封闭体系等热解实验。在数值模拟方面,基于化学动力学原理对烃源岩生烃过程开展了定量研究^[34-36]。在研究烃源岩生烃过程中所建立的理论、方法和模型仍然适用于页岩原位加热改质研究。国内外学者通过热解实验,确定了不同升温阶段页岩的热解产物组分,并根据产率的变化揭示了有机质初次和二次裂解的动力学特征^[19,37-40]。也有学者通过热重分析确定了不同升温阶段时页岩的重量损失,并逆向推断出不同升温阶段所对应的裂解作用以及该过程中的有机-无机裂解反应进程^[41-43]。

明确页岩孔隙演化规律是研究页岩油气储集空间和赋存状态的重要环节,为此,国内外学者通过对自然演化和热模拟催熟的页岩样品进行孔隙表征,以阐明页岩在不同热演化程度时的孔隙演化规律。对人工热催熟页岩样品的研究表明,低温氮吸附实验所测得的页岩比孔容在受热过程中明显增大,但增幅差异较大(图1)^[44]。在无围压条件下对页岩样品进行人工催熟处理,从低熟阶段到高熟阶段,伍德福德页岩、鄂尔多斯盆地延长组7段页岩、四川盆地二叠系页岩和中扬子寒武系水井沱组页岩比孔容可增大到原始样品的1.8~4.2倍,松辽盆地长岭凹陷嫩江组二段湖相页岩原始样品比孔容较小,仅为 $0.0065\text{ cm}^3/\text{g}$,当 R_o (镜质体反射率,最重要的有机质成熟度指标,用来标定从早期成岩作用直至深变质阶段有机质的热演化)达到1.37%时,比孔容陡增至 $0.0664\text{ cm}^3/\text{g}$,当 R_o 增至4.0%时,比孔容增加到原始样品的15.7倍^[29,45-48]。

另有学者对泥岩、页岩和油页岩加热至 $500\sim 650\text{ }^\circ\text{C}$,并对样品的比孔容和孔隙度进行测试,发现比孔容和孔隙度均随加热温度的增高而明显增大(图2)^[33,49-51]。其中,当温度高于 $300\text{ }^\circ\text{C}$ 时,抚顺油页岩和鄂尔多斯盆地长7段油页岩的比孔容急剧升高,当温度达到 $400\text{ }^\circ\text{C}$ 时,鄂尔多斯盆地泥岩孔隙度增幅明显变大,因此, $300\text{ }^\circ\text{C}$ 和 $400\text{ }^\circ\text{C}$ 可能分别为油页岩和泥岩

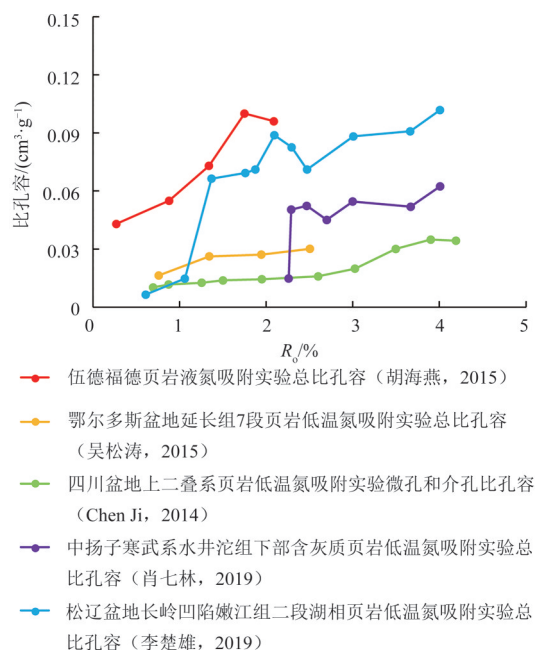
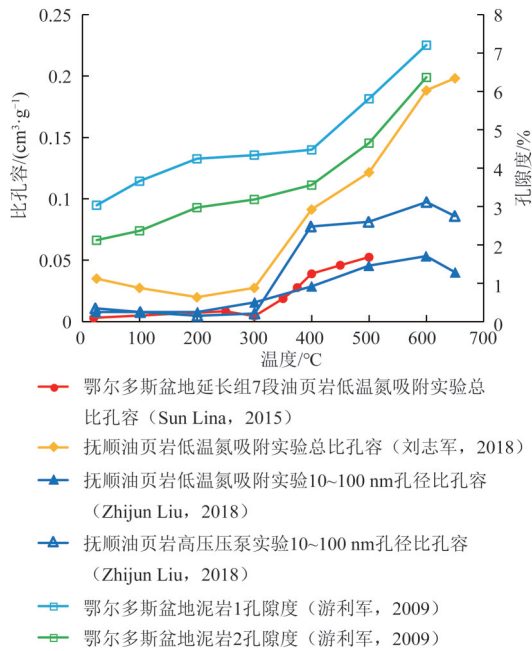


图1 人工热催熟页岩样品低温氮吸附实验所得比孔容变化对比^[29,45-48]

Fig. 1 Comparison of specific pore volume of artificial thermal mature shale samples obtained by nitrogen adsorption experiment at low temperature^[29,45-48]

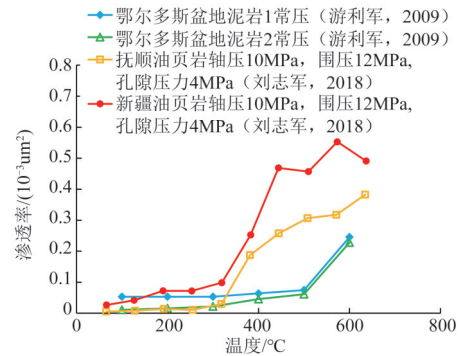
图2 比孔容和孔隙度随样品加热温度的变化^[33,49-51]Fig. 2 Specific pore volume and porosity variation in samples with different heating temperatures^[33,49-51]

热破裂的温度阈值。这种孔隙体积的变化主要由生排烃、热破裂和无机矿物演化等作用所造成^[51],但不同岩石性质可能造成温度阈值的差异性。

崔景伟在覆压条件下对样品进行加热催熟,发现孔隙体积随温度的增加而增大,但达到峰值后随温度的升高而降低,这可能由于部分有机孔隙在围压作用下被压实所致^[52]。不同学者的实验结果在微孔、介孔和宏孔的变化规律上不完全一致^[53-55],但在有机孔的贡献方面可基本达成一致,即认为有机质的生-排烃过程所导致的有机孔隙演化在页岩总孔隙演化过程中起到了至关重要的作用^[47,49,56-57],此外,无机矿物的成岩转化也是页岩储层性质改善的重要原因^[45-46]。

比孔容和孔隙度的增大,必然导致渗透率随之增大,实验结果显示,渗透率的变化与孔隙变化趋势具有一定相似性,抚顺油页岩和新疆油页岩样品渗透率在300℃左右开始大幅升高,而鄂尔多斯盆地泥岩样品渗透率则在450℃左右才开始大幅升高,油页岩和泥岩的渗透率变化温度阈值分别为300℃和450℃(图3)^[33,58]。

除热破裂效应之外,页岩因富含有机质而具有特殊性。在高温加热过程中,干酪根将发生初次裂解生成油气分子,已经生成的油气分子将发生二次裂解生成分子量更小的油气分子。这是一个油气分子数量逐渐增多,并且平均分子量逐渐降低的过程。该过程中流体体积膨胀系数逐渐增高,流体体积发生大幅度膨

图3 页岩在不同围压条件下加热到不同温度时的渗透率^[33,58]Fig. 3 Permeability of shale heated to different temperatures under different confining pressures^[33,58]

胀,在孔隙中形成生烃增压效应^[17,18,59-60]。有机碳含量为5%、氢指数为600 mg/g的页岩样品在封闭体系中进行热模拟实验,体系压力可增高至66 MPa^[61]。生烃增压效应所蓄积的流体压力将与热应力发生叠加,使热致裂作用进一步复杂化,对突破页岩矿物颗粒内部以及颗粒之间的连结力起到促进作用,进而加剧页岩的热致裂效应。因此,在研究页岩热致裂效应时,需将页岩矿物骨架的热破裂作用与生烃增压致裂作用进行耦合,综合研究页岩热致裂机理及其数值模拟方法,以达到对热致裂过程及其所伴随的孔渗变化进行动态定量预测的目的。

上述研究主要在关注有机质裂解生成油、气的过程,以及该过程中所伴随的有机质孔隙和粘土矿物孔隙演化,对高温高压条件下的酸性生烃附属产物(有机酸、H₂S和CO₂等)的生成及其对矿物产生的溶蚀作用和重结晶作用等成岩演化的影响研究相对薄弱,由该过程所导致的页岩储层增孔效果的量化研究有待进一步开展。

2.2 原位加热中页岩致裂效应

事实上,对于岩石热破裂作用的研究并非一个全新的课题。为了满足油气开发、地热能开发和核废料存储等领域的需求,前人已分别从实验室物理模拟、微观机理模拟和数值模拟等方面对砂岩、碳酸岩和花岗岩等岩石的热破裂现象开展了一定研究^[32,62-63]。

2.2.1 实验研究

实验方面,利用电液伺服材料试验系统进行温度加载,同时检测岩石渗透率的变化,以反映岩石的热破裂程度。与此同时,通过声发射记录仪实时检测各个温度段的岩石破裂声发射信号,包括声发射事件数、能量、持续时间和振幅等参量,用以监测不同温度时岩石

热破裂的进程和强度,并确定岩石热破裂的温度阈值^[32,63-64]。赵阳升等^[65]将细砂岩由 150 °C 加热到 300 °C,并在高温三轴应力条件下检测声发射事件(图 4),发现从 175 °C 开始,细砂岩声发射事件增多,在 185 ~ 203 °C 最为剧烈和密集,后间歇性减弱至 230 °C 进入相对平静期。

此外,通过对热处理过的岩石样品进行光学显微镜、扫描电镜、X 射线形貌和 CT 等实验,从微观角度研究了岩石热破裂过程中细纹萌生、扩展、贯通和失稳过程的规律以及孔裂隙结构演化规律^[66-67]。赵阳升等^[68]将花岗岩加热到不同温度后通过 CT 实验观测岩石的细观变化,加热到 500 °C 时,晶体颗粒的封闭多边形裂纹几乎全部形成,使花岗岩呈现糜棱状的晶体颗粒结构,90 % 以上的热破裂裂纹沿颗粒周边的相对薄弱的胶结界面发生,仅有少部分裂纹穿过岩石颗粒。

此外,也有学者对于油页岩原位加热改质过程中储层物性的变化开展了一定研究,比如太原理工大学对加热到不同阶段的油页岩进行 CT 扫描,得到了油页岩在热解过程中的整体破裂规律,认为油页岩热破裂的阈值温度为 200 ~ 300 °C (图 5),与前文所述低温氮吸附实验和氦气法孔隙度实验得到的结果一致^[69-72]。

奥斯陆大学的 Maya Kobchenko 等(2011)^[73]将绿河页岩从 60 °C 加热到 400 °C,采用 X 射线断层成像技术进行观测,结果显示,在 350 °C 左右开始产生裂缝,随着温度继续升高,平行于页岩层理的裂缝扩展合并(图 6)。

地质条件下的加热与实验室条件下的加热存在一定区别,主要体现在以下几个方面:①加热温度不同,地质条件下加热温度可能在 300 °C 或 350 °C 左右,而实验室中可达 600 °C;②升温速率不同,地质条件下页岩储层尺度大,升温速率很大程度上取决于岩石热传导效率,而实验室条件下页岩样品尺度小,升温速率快;③围压不同,地质条件下页岩储层处于地层压力下,而

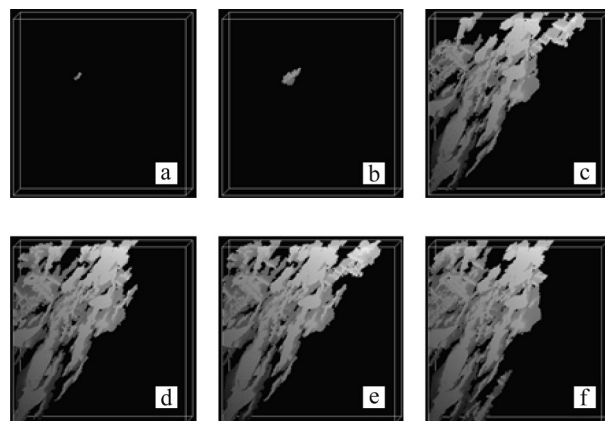


图 5 不同温度下油页岩内部最大空隙连通团分布^[72]

Fig. 5 Distribution diagrams of the largest pore groups connected in oil shale at different temperatures^[72]

a. $T=20\text{ }^{\circ}\text{C}$; b. $T=100\text{ }^{\circ}\text{C}$; c. $T=200\text{ }^{\circ}\text{C}$;
d. $T=300\text{ }^{\circ}\text{C}$; e. $T=400\text{ }^{\circ}\text{C}$; f. $T=500\text{ }^{\circ}\text{C}$

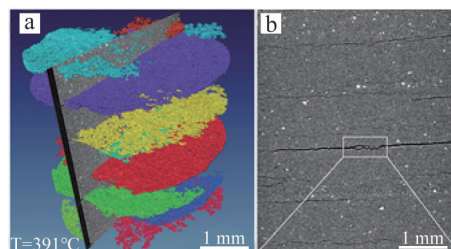


图 6 加热到 391 °C 时页岩样品 X 射线断层成像

Fig. 6 X-ray tomography images showing shale samples heated to 391 °C

a. 裂缝网络三维效果图,每种颜色代表一个独立裂纹; b. 二维切片

实验中可能在无围压条件下进行。

在实验室研究过程中,要在不同围压下进行加热,阐明围压对页岩起裂规律的影响,并且,以不同的升温速率将页岩加热到不同温度,以阐明升温速率和温度对页岩热破裂的影响。在进行地质评价时,需要综合考虑围压、加热温度和升温速率的影响,从实验室尺度跨度到地质尺度,以便做出客观准确的预测。

2.2.2 岩石热破裂细观机理研究

通过宏观实验往往只能获得岩石热破裂的宏观过程,难以揭示热破裂的细观机理。Cundall 率先提出可通过在颗粒流 (particle flow code, 简称 PFC) 离散元模拟中赋予模型热存储和热传导属性^[74-75],从而模拟岩石细观颗粒的力与运动状态,并进一步揭示岩石裂缝在热-力耦合作用下的热破裂细观机理。在构建基于岩石细观组分空间分布的 PFC 数值模型^[76]的基础上,进行单轴压缩模拟,确定模型力学参数。在充分考虑岩石力学与热力学参数的基础上进行升温模拟,阐明

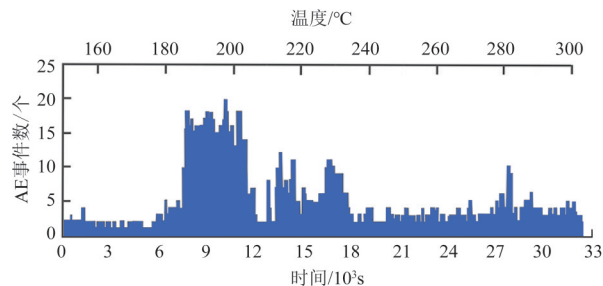


图 4 高温三轴应力条件下细砂岩声发射事件计数率^[65]

Fig. 4 Acoustic emission event counting rates of fine sandstone under high temperature triaxial stress^[65]

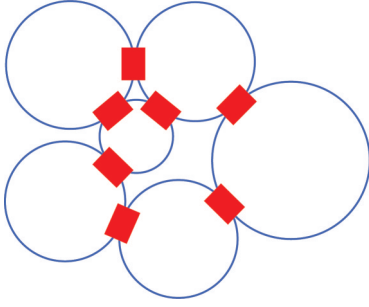


图7 平行粘结模型

Fig. 7 Parallel bond model

岩石应变、裂缝数量、裂缝分布形态等参数随温度升高的变化规律,以及应力对岩石热破裂的影响规律,进而揭示热破裂细观机理。PFC模拟中使用的所有本构方程均为接触方程,通常采用平行粘结模型表征岩石材料的胶结现象^[77-79](图7)。

在PFC模拟中,总接触力根据接触面可分为切向接触力和法向接触力^[80]:

$$\bar{F}_i = \bar{F}_i^n + \bar{F}_i^s \quad (1)$$

$$\bar{M}_i = \bar{M}_i^n + \bar{M}_i^s \quad (2)$$

式中: $\bar{F}_i^n$ 为力,N; $\bar{M}_i^n$ 为力矩的法向向量,N·m; $\bar{F}_i^s$ 为力,N; $\bar{M}_i^s$ 为力矩的切向分量,N·m。

平行粘结模型可以视为梁结构,根据梁理论^[81],在粘结周边会产生最大拉应力($\sigma_{\max}$)和最大剪应力($\tau_{\max}$):

$$\sigma_{\max} = \frac{-\bar{F}_i^n}{A} + \frac{|\bar{M}_i^n|}{I} \bar{R} \quad (3)$$

$$\tau_{\max} = \frac{\bar{F}_i^s}{A} + \frac{|\bar{M}_i^s|}{J} \bar{R} \quad (4)$$

式中: A 为粘结面的面积, m^2 ; J 为截面的极惯性矩, m^4 ; I 为截面切向的惯性矩, m^4 。

当最大拉应力大于平行粘结抗拉强度或者最大剪应力大于平行粘结抗剪强度时,颗粒连接键发生断裂,即在颗粒的粘结处产生裂纹。可根据拉破坏形成拉伸裂纹、剪破坏形成剪切裂纹的原则,判别优先产生哪种裂纹。

采用PFC模拟所揭示的岩石热破裂效应随温度变化的发展规律及其细观机理,将为进一步建立或优选模型对热破裂作用进行宏观预测提供理论基础和参数依据。

2.2.3 数值模拟研究

自从Dougill于1976年首次将损伤力学引入岩石类材料的研究领域以来^[82],有关岩石损伤特性的研究得到了学者们的广泛关注。通过高温条件下的力学和

显微观察等实验,得到岩石力学和热力学损伤规律,在此基础上建立或完善岩石损伤模型^[83-91],探究温度和压缩荷载共同作用下的岩石力学行为和破裂的宏观变化过程^[92-94]。

康健^[31]为探究高温地热资源开发中的岩石热破裂机制,采用随机概率分布函数(随机均匀分布、随机正态分布、随机韦伯分布、随机指数分布)对岩石非均质性进行描述,基于弹塑性理论^[95]建立随机非均质热弹塑性力学模型:

$$\begin{cases} \frac{\partial \sigma_{x_1}}{\partial x_1} + \frac{\partial \tau_{x_1 x_2}}{\partial x_2} + \frac{\partial \tau_{x_1 x_3}}{\partial x_3} + F_1 = \frac{\partial(3K\beta T)}{\partial x_1} \\ \frac{\partial \tau_{x_1 x_2}}{\partial x_1} + \frac{\partial \sigma_{x_2}}{\partial x_2} + \frac{\partial \tau_{x_2 x_3}}{\partial x_3} + F_2 = \frac{\partial(3K\beta T)}{\partial x_2} \\ \frac{\partial \tau_{x_1 x_3}}{\partial x_1} + \frac{\partial \tau_{x_2 x_3}}{\partial x_2} + \frac{\partial \sigma_{x_3}}{\partial x_3} + F_3 = \frac{\partial(3K\beta T)}{\partial x_3} \end{cases} \quad (5)$$

其中,

$$\sigma_{x_i} = \lambda \varepsilon + 2G \gamma_i = G \gamma_{x_i x_j} = G \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad (6)$$

$$\varepsilon = \varepsilon_{x_1} + \varepsilon_{x_2} + \varepsilon_{x_3} \quad (7)$$

$$\varepsilon_{x_i} = \frac{\partial u_i}{\partial x_i} \quad (i = 1, 2, 3) \quad (8)$$

式中: x_i 为坐标,无量纲, $i=1$ 为 x 方向, $i=2$ 为 y 方向, $i=3$ 为 z 方向; σ 为正应力,N; τ 为切应力,N; λ 和 G 为拉梅常数,无量纲; u 为位移,m; F 为外力,N; β 为热膨胀系数,无量纲; γ 为剪切应变,无量纲; ε 为体积应变,无量纲; K 为体积变形模量,无量纲; T 为温度,K。为了有针对性地考虑温度梯度和热膨胀梯度引起的岩石应变效应,将 λ 和 G 定为常数,可得岩体应力平衡方程:

$$(\lambda + G) \frac{\partial^2 u_j}{\partial x_i \partial x_j} + G \frac{\partial^2 u_i}{\partial x_j \partial x_j} + F_i = 3K \left(\beta \frac{\partial T}{\partial x_i} + T \frac{\partial \beta}{\partial x_i} \right) \quad (9)$$

与此同时,建立岩体随机介质非稳态热传导方程:

$$\kappa \nabla^2 T + \frac{\partial \kappa}{\partial x_1} \frac{\partial T}{\partial x_1} + \frac{\partial \kappa}{\partial x_2} \frac{\partial T}{\partial x_2} + \frac{\partial \kappa}{\partial x_3} \frac{\partial T}{\partial x_3} = \rho c \frac{\partial T}{\partial t} + c T \frac{\partial \rho}{\partial t} + \rho T \frac{\partial c}{\partial t} + Q_0 \quad (10)$$

式中: κ 为导热系数, $\text{W}/(\text{m} \cdot \text{K})$; ∇^2 为拉普拉斯算子,无量纲; T 为温度,K; ρ 为材料的密度, kg/m^3 ; c 为比热容, $\text{J}/(\text{K} \cdot \text{kg})$; t 为时间,s; Q_0 为体系的总热量,J。

将岩体应力平衡方程与随机介质非稳态热传导方程进行耦合,将力学参数(如弹性模量、泊松比、内摩擦角、抗拉强度、抗剪强度、抗压强度等)设为定值,采用有限元分析方法进行数值求解,得到热变形引起的初应变 ε_0 ,并进一步确定初应变引起的等效节点载荷 F_T

和 F_{β} 。采用Drucker-Prager屈服准则^[96]对热破裂进行判定,根据逾渗理论^[97-104],当平面模型热破裂的单元数达到59.275%时,即认为对应的温度为热破裂阈值 T_c ,亦可考察此时岩石渗透率的突变情况。并可通过对随机分布函数及其参数的调整,考察岩石非均质性对热破裂作用的影响。通过数值模拟探索岩石受热时裂纹产生、扩展、汇合以及贯通过程的变化规律。

对上述研究思路进行延伸,进一步探索破裂单元比例与渗透率之间的关系,并根据破裂单元比例的变化评价渗透率在热破裂过程中的变化过程,有望据此对原位加热过程中的页岩渗透率进行预测。

前期对于砂岩、碳酸盐岩和花岗岩等岩石热破裂作用的研究无疑为页岩的研究奠定了良好基础,不难将其实验方法、理论模拟和数学模型进行有针对性的改进和转化,服务于页岩热破裂作用的研究。但页岩具有其特殊性,比如在受热过程中将因有机质裂解而产生增压致裂效应,在研究过程中应特别加强对该过程的关注。

3 结语

基于对有机-无机成岩作用和热致裂效应的分析,初步明确了页岩原位加热过程中储层改质效应的主要机理,即由有机质裂解、无机矿物转化、矿物溶蚀和重结晶引起的孔隙演化效应,以及由热应力和生烃增压所造成的致裂效应耦合所导致。增孔和致裂效应叠加,将导致页岩储层孔渗条件大幅改善,是页岩油原位加热增产的重要理论基础之一。

尽管目前对于加热后页岩的孔隙演化开展了一定研究,但基本上是对增孔致裂综合效应的整体分析,未对有机、无机孔隙演化以及热破裂和生烃增压致裂过程分别开展研究。这意味着对增孔致裂机理的认识仍不充分,无法从机理出发对单一过程进行准确预测,更无法实现对整个增孔增渗过程的准确预测。因此,在进一步研究中需对有机、无机孔隙演化和热破裂、生烃增压致裂开展相对独立的研究,分别揭示其机理并建立评价模型。在与热传导模型耦合的基础上,实现对原位加热过程中增孔增渗效应在时间和空间上的定量预测,为开发方案的制定奠定基础。

此外,不同构造和沉积背景的含油气盆地或同一含油气盆地的不同沉积(微)相中页岩的岩相具有显著差异,意味着页岩在有机质含量与性质、无机矿物组成和储层孔隙度、渗透率、孔隙结构等方面存在明显差异。岩相的多样性必将导致受热过程中生排烃、无机

矿物转化、热破裂和增压致裂等效应的明显差异,进而影响整体增压致裂效果。因此,对不同岩相的页岩分别开展增压致裂机理研究,对该效应的工程预测具有现实意义。

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